

# Bicubic splines for fast-contracting control nets

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**Abstract:** Merging parallel quad strips facilitates narrowing surface passages, and allows a design to transition to simpler shape. While a number of spline surface constructions exist for the isotropic case where  $n$  pieces join, few existing spline constructions deliver good shape for control-nets that merge parameter lines; and, until recently, none provided good shape for fast-contracting polyhedral control-nets. This work improves the state-of-the-art of piecewise polynomial spline surfaces accommodating fast-contracting control nets. The new fast-contracting (FC) surface algorithm yields the industry-preferred uniform degree bi-3 (bi-cubic), the surfaces are by default differentiable, have improved shape, measured empirically as highlight line distribution, and require fewer pieces than the state-of-the-art.

**Keywords:** polyhedral-net spline; control-net contraction; geometric continuity

**MSC:** 68U07 Computer science aspects of computer-aided design, 65D17 Computer-aided design (modeling of curves and surfaces)

## 1. Introduction

To accommodate narrower surface passages or account for less shape fluctuation, a designer can merge parallel parameter lines as illustrated in Fig. 1 a,b, see the gray regions. Aggressive merging in quad-meshing algorithms such as [1,2] packs the gray contraction regions too close to each other as in Fig. 1 c,d: existing algorithms require these faces to be separated by a frame of quadrilaterals. Mitigation strategies range from ad hoc designer intervention, to an improved Doo-Sabin refinement step [3,4], to special re-meshing rules for  $T_0$ - and  $T_1$ -locations, [5], see Fig. 1 e. The drawback of these mitigations is both an increase in the number of patches and a decrease in the surface quality. Surface quality suffers since, to obtain the required combinatorial structure, the natural cross field (flow) of the geometry is disturbed.

The recent publication [6] therefore presented two new Fast Contracting (FC) spline constructions:  $FC^4$  and  $FC^3$ .  $FC^4$  generates surfaces of bi-degree (2, 4) or (2, 3),  $FC^3$  of bi-degree 3. Both assume that the regular quad-grid of the control net define bi-2  $C^1$  splines, and both use as control net the un-isotropic  $\Delta^2$  configuration of Fig. 1 f, that retains the two preferred directions of the tensor-product splines. The split of the gray core is ignored and no re-meshing or refinement is required to guarantee geometric  $G^1$  continuity of the resulting surfaces.

Unlike  $FC^3$ , the new bi-3 construction  $FC_8^3$  manages the transition from two (top) to four (bottom) bi-3 pieces via two internal T-junctions, and requires only the two T-junctions of the center line, see Fig. 2 (e) vs (f). Remarkably,

- $FC_8^3$  is a 8-piece bi-3 (bi-cubic) construction.
- $FC_8^3$  yields improved shape compared to  $FC^3$ , measured empirically as more uniform highlight line distribution, and has fewer polynomial pieces, the minimal number required for good shape.
- The  $FC_8^3$  formulas for generating bi-3 patches are linear in the input control net, hence can be collected into a matrix.
- Implementation of  $FC_8^3$  can so be reduced to: gathering the control net in a vector of points and multiplying the vector by a matrix.

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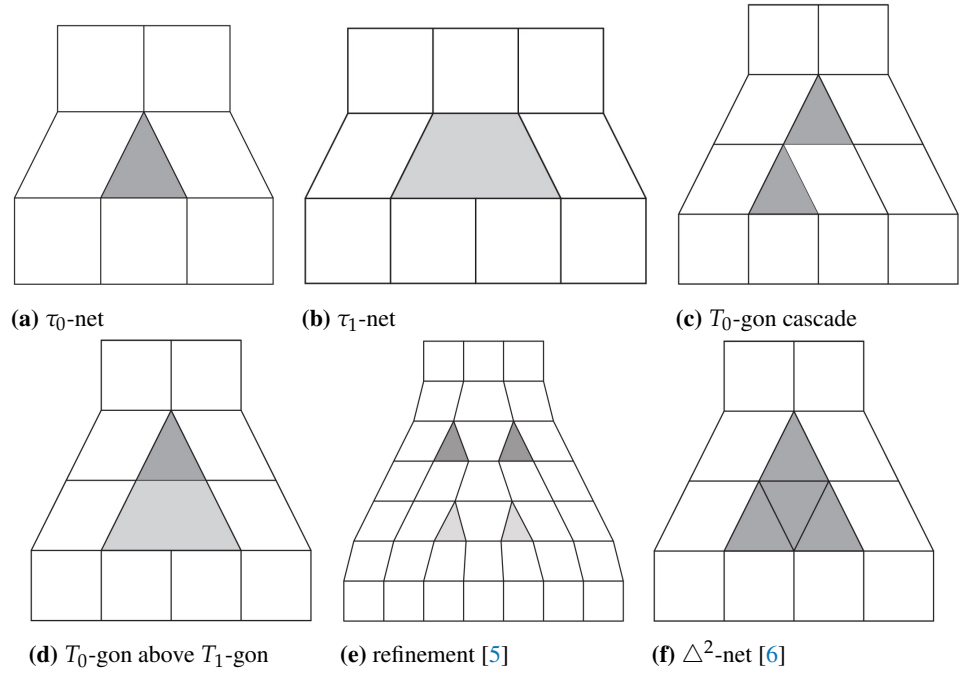
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**Figure 1.** Contracting control-net configurations: one strip contraction in a (a)  $\tau_0$ -net and (b)  $\tau_1$ -net from [7,8] and two-strip contraction via (c) cascading triangles, (d)  $T_0$ -gon +  $T_1$ -gon and (e) refinement according [5]; (f)  $\Delta^2$ -net with triangulated gray core as a generalization of (c) and (d): removing from the core one inner bottom edge yields (c), removing both yields (d).

The patch count can be further reduced to 7 by merging the two middle patches of  $FC_8^3$ , but, as is demonstrated, this diminishes the resulting surface quality significantly.

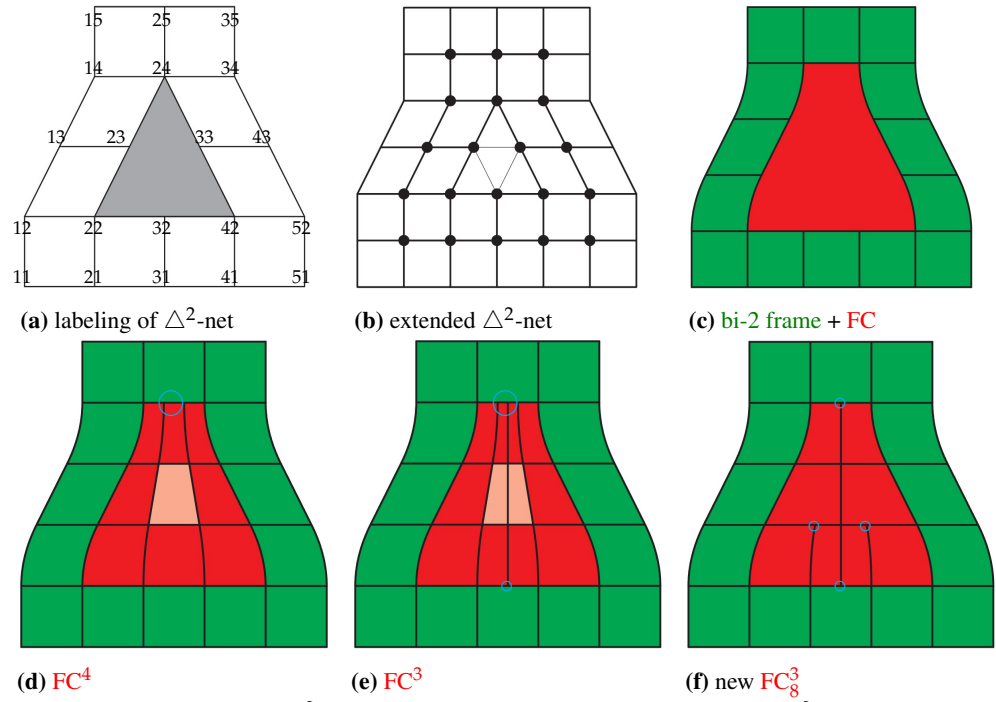
We note that tensor product splines (NURBS) are the preferred representation in many modeling packages and degree bi-3 (bi-cubic) is the preferred degree. Catmull-Clark subdivision surfaces [9], popular in computer graphics, are also of degree bi-3 but consist of an infinite sequence of nested rings generated by recursion. More importantly however, Catmull-Clark and bi-2 Doo-Sabin [3] subdivision rules, are for treating control net configurations with  $n$  directions equally, i.e. *isotropically*, whereas FC splines retain the two preferred direction of the bivariate tensor-product splines. That is, FC splines are more general than tensor-products in that they allow merging of quad strips.

After a brief literature review, Section 2 introduces the technical nomenclature and reviews the existing constructions  $FC^3$  and  $FC^4$ . Section 3 introduces and derives the new  $\Delta^2$ -net construction with explicit tables for implementation. Section 4 provides example-driven critical assessment and discussion of variants as well a comparison to  $FC^3$ . For rotationally-symmetric scenarios that permit regular layout or less contraction  $FC_8^3$  is shown to be at least as well-shaped as regular bi-2 splines and the surfaces of [8].

### 1.1. Related work

FC constructions assemble a finite number of polynomial pieces to join smoothly after a change of variables. Such  $G^k$  constructions complement constructions for isotropic configurations such as rational multi-sided surfaces [10–12], and singularly parameterized surfaces. The sub-genres of singular constructions are subdivision surfaces [3,9,13,13–15], edge collapse, polar surfaces [16–18], and vertex singular surfaces [19–22] or rational singular constructions [23,24].

The shape of  $G^2$  constructions of degree bi-7 [25] or degree bi-6 [26], and lower-degree tangent-continuous splines [27–33] is empirically measured via highlight line distribution, [34]. FC surfaces fill irregularities in a  $C^1$  bi-quadratic (bi-2) tensor-product surface, which is attractive since bi-2 splines have minimal bi-degree for smoothing quadrilateral meshes. Subdivision generalizations of bi-2 splines consist of an infinite sequence of nested (contracting) bi-2 polynomial surface rings. [3] has visible artifacts already in the first ring, Augmented Subdivision [4] improves shape by



**Figure 2.** Rapid contraction: (a)  $\Delta^2$ -net with 20 labels of its nodes  $d_{ij}$ . (b) Extended  $\Delta^2$ -net allows to produce via B-to-BB conversion one bi-2 frame as shown in (c,d,e,f). Bottom row: layouts of  $FC^4$  and  $FC^3$  from [6] and  $FC_8^3$ .

following a carefully chosen central guide point and Polyhedral-net Splines [35] combine algorithms from [18,36,37] to generalize tensor-product bi-quadratic (bi-2) splines, filling in a *finitely many* polynomial pieces of degree at most bi-3. T-splines [38] address the merging parallel quad strips but typically serve only to refine an existing quad partition: due to their global parameterization requirement, they may not be well-defined for a given T-configuration, see [39, Fig 2], [40, Fig 6]. Alternatively, T-junctions in the control net can be associated with smooth surfaces of bi-degree (2, 4) ([7]) or bi-3 ([8]) that result in smooth surfaces of good quality.  $FC_8^3$  is partly motivated by the output of quad-dominant meshing algorithms such as [1,2], that introduce (fast) mesh contractions. We note, that the present paper does not touch re-meshing [41–43], but focuses on frequently occurring contracting configurations.

## 2. Control nets, macro-patches, $FC^3$ and $FC^4$

$FC_8^3$  is an improvement of  $FC^3$ . We therefore use the notation of [6]. As do tensor-product spline control nets the  $\Delta^2$  nets have two distinguished directions that we refer to as ‘vertical’ and ‘horizontal’ due to their layout in Fig. 2. The number of mesh lines is reduced or expanded only in the vertical direction.

### 2.1. Control nets

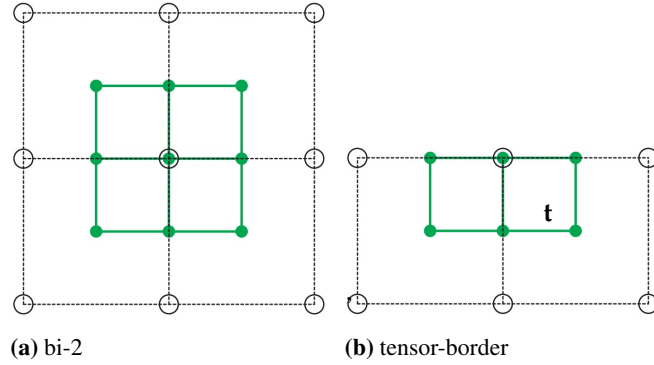
Fig. 2a displays the labels of  $\Delta^2$ -net used for derivation and presentation of pre-calculated data. The bottom row of Fig. 2 compares the patchworks of three  $FC$  surfaces.  $FC^4$ , see Fig. 2d, consists of pieces of bi-degree (2, 4) (i.e. 2 in the horizontal direction) except for a middle row of bi-degree (2, 3). The central, light-red patch serves as a model for the bi-3 constructions. For  $FC^3$ , see Fig. 2e, this central patch is degree-raised to bi-3 and split into two to keep a tensor-product structure of red macro-patch. The layout of the bi-3 pieces of  $FC_8^3$  is shown in Fig. 2f. The circles in Fig. 2(d,e,f) mark the locations of T-junctions: small  $\circ$  points to a single T-junction,  $\bigcirc$  to multiple T-junctions. The two T-junctions in (d) merge three strips into one. The additional T-junctions in (e) follow from the fact, proven in [6], that any  $C^1$  bi-3 construction requires an even number of pieces, both at the bottom and the top.

## 2.2. Polynomial pieces

$FC_8^3$  consists of tensor-product pieces of polynomial bi-degree  $(d, d')$  in Bernstein-Bézier form (*BB-form*, [44]). That is, for Bernstein polynomials  $B_k^d(t) := \binom{d}{k}(1-t)^{d-k}t^k$ , the bi-degree 3 (bi-3) patch  $\mathbf{p}$  is defined as

$$\mathbf{p}(u, v) := \sum_{i=0}^3 \sum_{j=0}^3 \mathbf{p}_{ij} B_i^3(u) B_j^3(v), \quad 0 \leq u, v \leq 1.$$

With the convention that  $u$  is the parameter tracing out the horizontal direction.



**Figure 3.** B-to-BB conversion and tensor-borders  $\mathbf{t}$  as Hermite input data. Circles  $\circ$  mark B-spline control points, solid disks  $\bullet$  mark BB-coefficients of the full patch, respectively tensor-border.

Connecting the *BB-coefficients*  $\mathbf{p}_{ij} \in \mathbb{R}^3$  to  $\mathbf{p}_{i+1,j}$  and  $\mathbf{p}_{i,j+1}$  wherever well-defined yields the *BB-net*, see Fig. 3. Any  $3 \times 3$  grid can be interpreted as the control net of a uniform bi-2 spline in uniform knot B-spline form. In Fig. 3 the B-spline control points are marked  $\circ$ . The *B-to-BB conversion* (e.g. by knot insertion) expresses the spline in bi-2 BB-form illustrated by the green BB-nets in Fig. 3. Conversion of a partial sub-grid yields a partial BB-net  $\mathbf{t}$ , called *tensor-border*, that defines position and first derivatives across an edge.

The changing number of mesh lines forces a change of parameterization and hence introduction of *geometric continuity*: Two polynomial pieces  $\mathbf{p}, \mathbf{q} : \mathbb{R}^2 \rightarrow \mathbb{R}^3$  join  $G^1$  along the common curve with BB-coefficients  $\mathbf{p}_{i0} = \mathbf{q}_{i0}$  if there exists a reparameterization  $\rho : \mathbb{R}^2 \rightarrow \mathbb{R}^2$ , see e.g. [45],

$$\mathbf{p}(u, v) := \mathbf{q} \circ \rho(u, v), \quad \rho(u, v) := (u + b(u)v, a(u)v) \quad (1)$$

$$\partial_v \mathbf{q}(u, 0) = a(u) \partial_v \mathbf{p}(u, 0) + b(u) \partial_u \mathbf{p}(u, 0) \quad (2)$$

for scalar-valued, univariate functions  $a$  and  $b$ . Besides the shared BB-coefficients of the common boundary, only the layers of BB-coefficients  $\mathbf{p}_{i1}$  and  $\mathbf{q}_{i1}$  of adjacent patches enter the  $G^1$  continuity constraints. In the derivation,  $u$ -,  $v$ -directions can be assigned as convenient, but typically  $u$  is used to parameterize along the boundary and  $v$  in the orthogonal direction of the tensor-border, towards the interior or core.

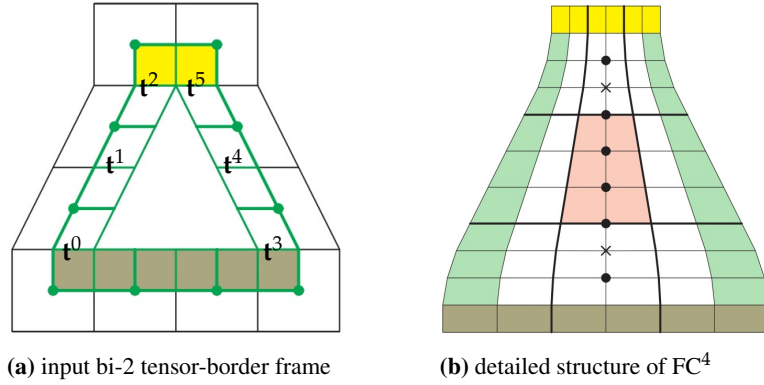
## 2.3. Summary of $FC^4$ and $FC^3$

The bi-2 tensor-border frame (darkgreen in Fig. 4 a) represents first-order Hermite data. This input for all FC constructions stems from the  $\Delta^2$ -net by B-to-BB conversion.

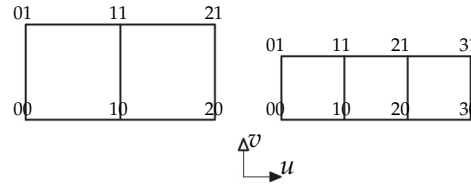
Fig. 4 summarizes the construction of  $FC^4$ . The khaki-colored bottom layer in (a) is degree-raised to bi-degree  $(2, 4)$  and the yellow top layer is uniformly split into 3 pieces and degree-raised. The light-green left and right layers are the result of reparameterizing the left pieces  $\mathbf{t}^0, \mathbf{t}^1, \mathbf{t}^2$ , respectively the right pieces  $\mathbf{t}^3, \mathbf{t}^4, \mathbf{t}^5$  of input tensor-border frame. Unconstrained BB-coefficients, are marked  $\bullet$ , and the BB-coefficients marked  $\times$  are defined by  $C^1$  extension of the central (light-red) patch. The remaining BB-coefficients are the averages of their horizontal (black and light-green) neighbor BB-coefficients.

The construction of  $FC^3$  is summarized in Fig. 6. In (a), leaving  $\mathbf{t}_i, i = 0, \dots, 5$ , from Fig. 4 a and  $\mathbf{t}_0$  and  $\mathbf{t}_3$  unchanged.  $\mathbf{t}_1$  and  $\mathbf{t}_2$  represent a uniformly split piece at the middle of the bottom





**Figure 4.**  $FC^4$  review: (a)  $\Delta^2$ -net and input bi-2 tensor-border frame obtained from  $\Delta^2$ -net by B-to-BB conversion. (b)  $3 \times 3$  macro-patch structure in BB-form.



**Figure 5.** Labeling of: *left* – bi-2 tensor-border; *right* – reparameterized bi-3 tensor-border.

frame of Fig. 4 a. Mimicking the bottom split,  $\bar{t}_i, i = 0, \dots, 3$ , top split with ratio  $1 : \frac{1}{2} : \frac{1}{2} : 1$ . In (b), the reparameterized pieces  $\bar{t}_i, i = 0, \dots, 5$ ,  $\underline{t}_i, i = 0, \dots, 3$  and  $\bar{t}_i, i = 0, \dots, 3$  (light-green) are consistent at all four corners and the light-red bi-3 patches 6 and 7 represent the central light-red bi-degree (2,3) patch from Fig. 4 b, after-degree raising and split. The reparameterizations  $\rho^s, s = 0, 1, 2$ ,  $\underline{\rho}^s, s = 0, 1, 2, 3$  and  $\bar{\rho}^s, s = 0, 1$  are also used in  $FC^3$  construction, see Fig. 5 for the labeling. Formulas (3) and (4) define the bi-3 tensor-border frame (light-green in Fig. 6 b) due to the symmetries  $\rho^{3+s} := \rho^s, s = 0, 1, 2$ .

$$\begin{aligned} \rho^s(u, v) &:= (u, a^s(u)), \quad a^s(u) := a_0^s(1 - u) + a_1^s u; \quad \tilde{t}^s := t^s \circ \rho^s; \\ [a_0^0, a_1^0] &:= [1, \frac{7}{9}], \quad [a_0^1, a_1^1] := [\frac{7}{9}, \frac{5}{9}], \quad [a_0^2, a_1^2] := [\frac{5}{9}, \frac{1}{3}]; \\ \tilde{t}_{01}^s &:= (1 - \frac{2}{3}a_0^s)t_{00}^s + \frac{2}{3}a_0^s t_{01}^s, \\ \tilde{t}_{11}^s &:= (\frac{1}{3} - \frac{2}{9}a_1^s)t_{00}^s + (\frac{2}{3} - \frac{4}{9}a_0^s)t_{10}^s + \frac{2}{9}a_1^s t_{01}^s + \frac{4}{9}a_0^s t_{11}^s. \end{aligned} \quad (3)$$

The boundary BB-coefficients  $\tilde{t}_{i0}^s, i = 0, \dots, 3$ , are obtained from  $t_i^s, i = 0, 1, 2$  by degree-raising. The remaining BB-coefficients  $t_{21}^s$  and  $t_{31}^s$  are defined by the symmetry  $t_{ij}^s \leftrightarrow t_{2-i,j}^s, i = 0, 1, 2, j = 0, 1; a_i^s \leftrightarrow a_{1-i}^s, i = 0, 1$ .

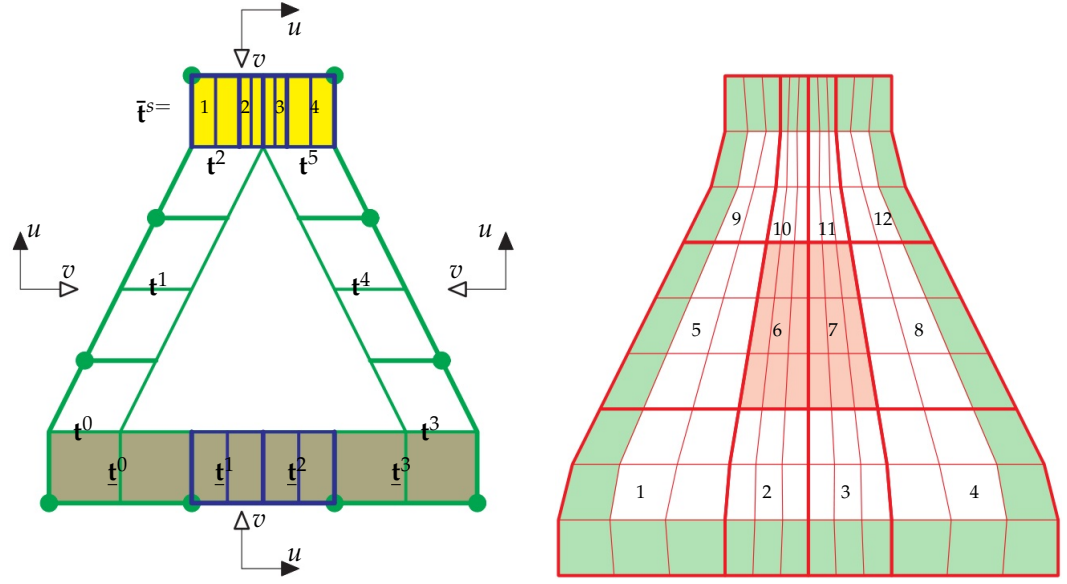
The bottom reparameterizations  $\underline{\rho}^s$  and top reparameterizations  $\bar{\rho}^s, s = 0, 1, 2, 3$ , are defined by formulas

$$\underline{\rho}^s := (u + \underline{\gamma}^s B_1^2(u)v, v), \quad \underline{\gamma}^s := \frac{(-1)^{s+1}}{9}; \quad \bar{\rho}^s := (u + \bar{\gamma}^s B_1^2(u)v, v), \quad \bar{\gamma}^s := \frac{(-1)^s}{3}.$$

Setting  $\gamma := \underline{\gamma}^s, \mathbf{p} := \underline{t}^s, \mathbf{q} := \tilde{t}^s$  in (4), yields explicit formulas for the BB-coefficients of the reparameterized bi-3 tensor-border  $\tilde{t}^s := t^s \circ \underline{\rho}^s$ . Setting  $\gamma := \bar{\gamma}^s, \mathbf{p} := \bar{t}^s, \mathbf{q} := \tilde{t}^s$  in (4) yields  $\tilde{t}^s := \bar{t}^s \circ \bar{\rho}^s$ .

$$\begin{aligned} \mathbf{q}_{01} &:= \frac{1}{3}\mathbf{p}_{00} + \frac{2}{3}\mathbf{p}_{01}, \quad \mathbf{q}_{31} := \frac{1}{3}\mathbf{p}_{20} + \frac{2}{3}\mathbf{p}_{21}, \\ \mathbf{q}_{11} &:= (\frac{1}{9} - \frac{4}{9}\gamma)\mathbf{p}_{00} + (\frac{2}{9} + \frac{4}{9}\gamma)\mathbf{p}_{10} + \frac{2}{9}\mathbf{p}_{01} + \frac{4}{9}\mathbf{p}_{11}, \\ \mathbf{q}_{21} &:= (\frac{2}{9} - \frac{4}{9}\gamma)\mathbf{p}_{10} + (\frac{1}{9} + \frac{4}{9}\gamma)\mathbf{p}_{20} + \frac{4}{9}\mathbf{p}_{11} + \frac{2}{9}\mathbf{p}_{21}, \end{aligned} \quad (4)$$

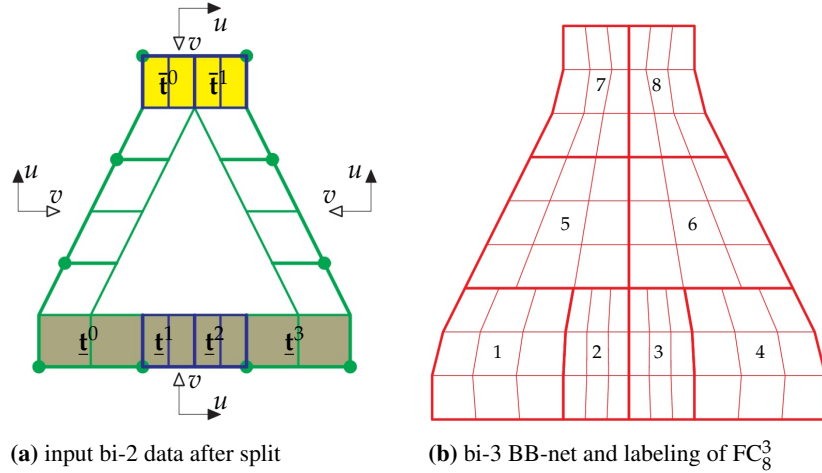
the boundary BB-coefficients  $\mathbf{q}_{i0}$ ,  $i = 0, 1, 2, 3$ , are obtained from  $\mathbf{p}_{i0}$ ,  $i = 0, 1, 2$ , by degree-raising. 138



(a) input bi-2 frame after split

(b) bi-3 BB-net of  $FC^3$

**Figure 6.**  $FC^3$ : (a) The input bi-2 frame is split (see blue top, bottom). The local  $u-v$ -coordinate systems of the tensor-borders are shown. (b) Layout of patches and BB-nets of  $FC^3$ .



(a) input bi-2 data after split

(b) bi-3 BB-net and labeling of  $FC_8^3$

**Figure 7.**  $FC_8^3$ : (a) The bi-2 tensor-border frame required for  $FC_8^3$  coincides with the frame in Fig. 6 a except at the top (yellow) that is *uniformly* split into two pieces. (b) BB-net and labeling of the  $FC_8^3$  macro-patch.

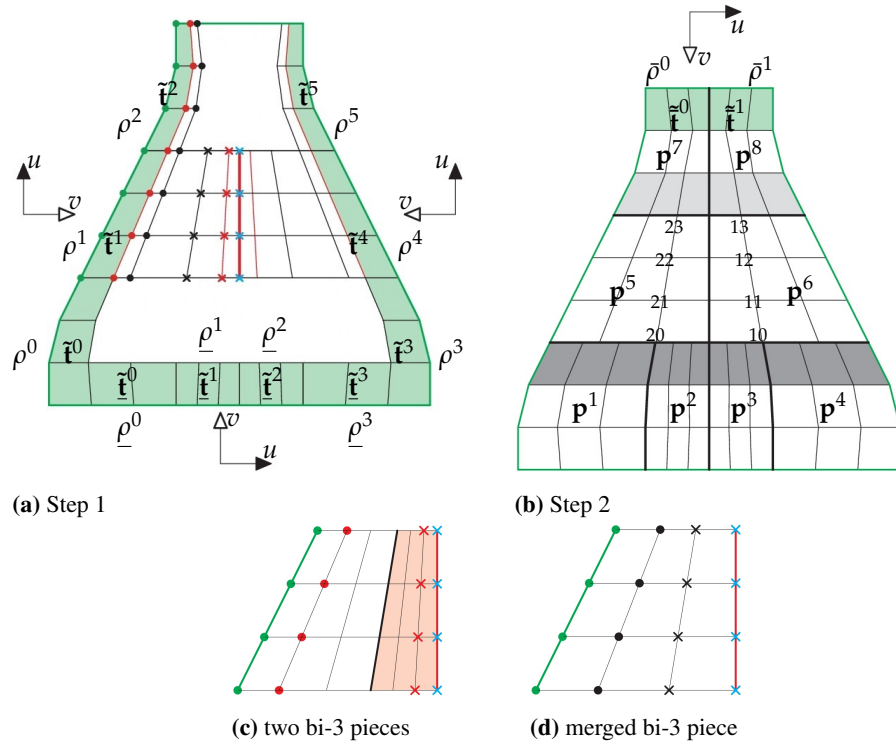
### 3. The $FC_8^3$ construction

Starting with the bi-2 tensor-border frame, see Fig. 7 a, of  $FC^3$ , cf. Fig. 6 a, but, anticipating the layout displayed in Fig. 7 b, *uniformly* splitting the top, we construct the bi-3 tensor-border frame (light-green in (a)) according to Section 2.3, Fig. 6, and the reparameterized tensor-borders  $\bar{t}^1, \bar{t}^2$  (and analogously  $\bar{t}^4, \bar{t}^5$ ) in Fig. 8 a re-scaled as  $\bullet := \frac{3}{2} \bullet - \frac{1}{2} \bullet$  (Hermite data:  $\bullet$  on the boundary remain unchanged). All data of  $\mathbf{p}^5$  in Fig. 8 b is displayed in Fig. 8 a, middle-left and again, enlarged, in Fig. 8 c,d: The light-red underlaid piece in Fig. 8 c represents bi-3 patch in Fig. 6 b with label 6. Leaving  $\times$  unchanged, we set the BB-coefficients marked  $\times := 3 \times - 2 \times$ , to form the layer  $\mathbf{p}_{2j}^5$ ,  $j = 0, \dots, 3$  in Fig. 8 b. The BB-coefficients  $\mathbf{p}_{1j}^6$ ,  $j = 0, \dots, 3$  are constructed analogously. By construction,  $\mathbf{p}_{3j}^5 = \mathbf{p}_{0j}^6$ ,  $j = 0, \dots, 3$  and  $\mathbf{p}_{3j}^5 := \frac{1}{2}\mathbf{p}_{2j}^5 + \frac{1}{2}\mathbf{p}_{1j}^6$ . On top, the re-scaled tensor-border is reparameterized by  $\bar{\rho}_0, \bar{\rho}_1$  defined in Section 2.3 yielding  $\bar{t}_0, \bar{t}_1$ , see Fig. 7 a. By inspection, the parameterization are consistent at the top two corners in Fig. 8 b. The patches  $\mathbf{p}^7$  and  $\mathbf{p}^8$  are

completed by light-gray extension of patches  $\mathbf{p}^5, \mathbf{p}^6$ , see Fig. 8 b. The patches  $\mathbf{p}^s, s = 1, \dots, 4$ , are completed by dark-gray extension of patches  $\mathbf{p}^5, \mathbf{p}^6$  and a subsequent split.

$\text{FC}_8^3$  expresses the BB-coefficients as an affine combinations of the  $\triangle^2$ -net nodes  $\mathbf{d}$ . That is, with the formulas of Section 2.3 explicit formulas are available once the BB-coefficients of the central patches are known (light-red in Fig. 6 b). These can be gleaned from [6], but here we present the explicit weights  $\mu$  of formulas formulas for  $j = 0, \dots, 3, s = 0, \dots, 3$  (see Fig. 8 b)

$$\begin{aligned} \mathbf{p}_{2s}^5 &:= \sum_{i=1}^5 \sum_{j=1}^2 \mu_{ij}^s \mathbf{d}_{ij} + \sum_{i=1}^4 \mu_{i3}^s \mathbf{d}_{i3} + \sum_{i=1}^3 \mu_{i4}^s \mathbf{d}_{i4}, \\ \mathbf{p}_{1s}^6 &:= \sum_{i=1}^5 \sum_{j=1}^2 \mu_{6-i,j}^s \mathbf{d}_{ij} + \sum_{i=1}^4 \mu_{5-i,3}^s \mathbf{d}_{i3} + \sum_{i=1}^3 \mu_{4-i,4}^s \mathbf{d}_{i4}. \end{aligned} \quad (5)$$



**Figure 8.** Derivation of the  $\text{FC}_8^3$  macro-patch construction and hence of the matrix that defines  $\text{FC}_8^3$ . Once derived, the implementation of  $\text{FC}_8^3$  is just a matrix multiplication.

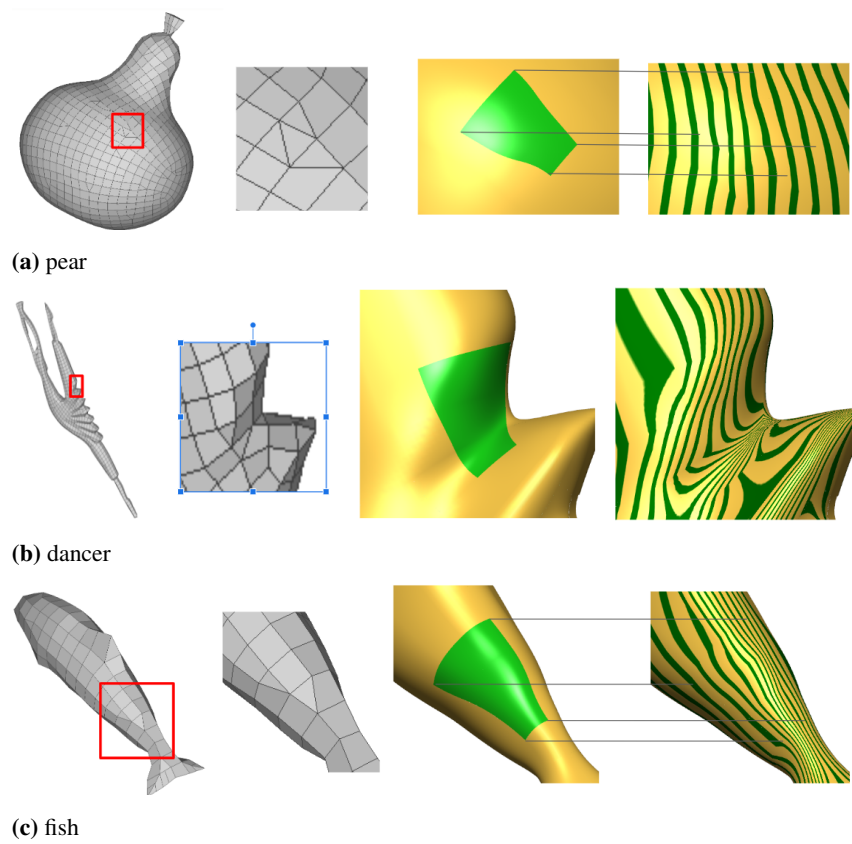
Without loss of quality, the coefficients  $\mu$  can be stated with 5 decimals accuracy and corrected by less than 0.00009 to form a partition of 1. That is, the weights  $\mu_{ij}^s$  listed below are exact, not approximations of the implementation weights.

Table  $M^s$  lists  $10^5 \begin{pmatrix} \mu_{14}^s & \mu_{24}^s & \mu_{34}^s & \times & \times \\ \mu_{13}^s & \mu_{23}^s & \mu_{33}^s & \mu_{43}^s & \times \\ \mu_{12}^s & \mu_{22}^s & \mu_{32}^s & \mu_{42}^s & \mu_{52}^s \\ \mu_{11}^s & \mu_{21}^s & \mu_{31}^s & \mu_{41}^s & \mu_{51}^s \end{pmatrix}.$

$$\begin{aligned} M^0 &:= \begin{pmatrix} 1287 & -2571 & 1287 & \times & \times \\ -896 & 38395 & 15479 & -2979 & \times \\ 4441 & 9437 & 47248 & -13479 & 2358 \\ -428 & 1705 & -2561 & 1705 & -428 \end{pmatrix}, M^1 := \begin{pmatrix} 1952 & -3904 & 1952 & \times & \times \\ 496 & 62003 & 25198 & -4364 & \times \\ 6080 & -9877 & 32592 & -16127 & 3997 \\ -934 & 3739 & -5608 & 3739 & -934 \end{pmatrix}, \\ M^2 &:= \begin{pmatrix} 2448 & 12463 & 1753 & \times & \times \\ 6449 & 56051 & 23412 & -2578 & \times \\ 2892 & -12303 & 18821 & -12303 & 2892 \\ -828 & 3315 & -4971 & 3315 & -828 \end{pmatrix}, M^3 := \begin{pmatrix} 8725 & 38797 & 2475 & \times & \times \\ 5059 & 32439 & 13689 & -1190 & \times \\ 1674 & -7179 & 11010 & -7179 & 1674 \\ -531 & 2128 & -3188 & 2128 & -531 \end{pmatrix}. \end{aligned}$$

#### 4. Assessments and Comparisons

One motivation of  $\text{FC}_8^3$  was to significantly reduce the number of bi-3 patches in  $\text{FC}^3$  without overtly harming surface quality. For completeness, we also compare with FP7, a FC construction

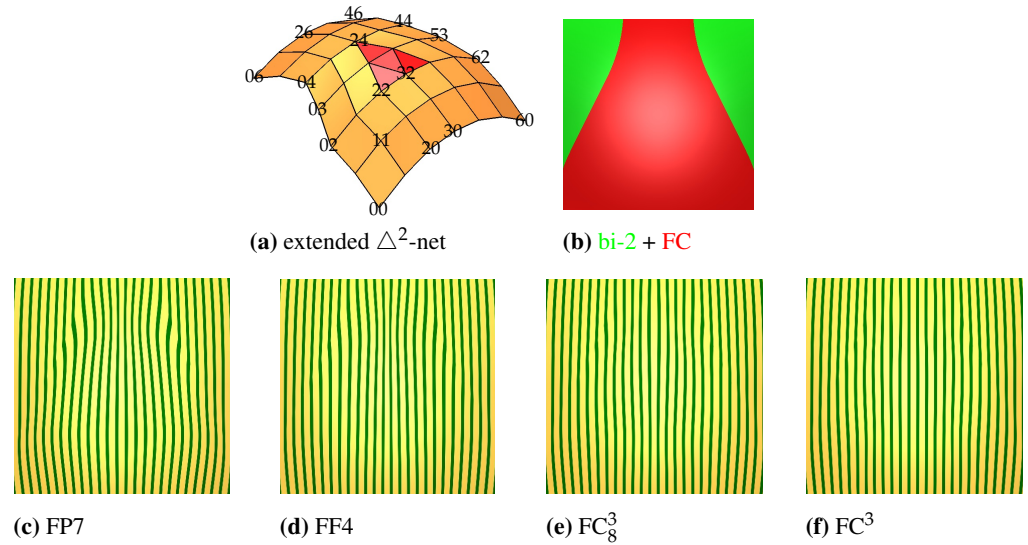


**Figure 9.**  $\triangle^2$ -nets arising in quad-dominant meshing 'in the wild'. Here  $FC_8^3$  is green. Models from [www.quadmesh.cloud/Thingi10K](http://www.quadmesh.cloud/Thingi10K) [46].

composed of 7 patches, and with FF4, of the same layout as  $FC_8^3$ , but pinning down degrees of freedom via the functional  $\mathcal{F}_4 := \int_0^1 \int_0^1 \sum_{i+j=4, i,j \geq 0} \frac{4!}{i!j!} (\partial_s^i \partial_t^j f(s, t))^2 ds dt$ .

#### 4.1. Small local challenge nets

Fig. 2 b already introduced the  $\triangle^2$ -net (nodes marked by  $\bullet$ ) extended by a quad frame whose outermost nodes can be of any valence. While a FC surface is fully defined by  $\triangle^2$ -net, the extended  $\triangle^2$ -net yields a regular B-spline **bi-2 frame** as in Fig. 2 c, and (d,e,f), that reveals any problems in the transition from regular to FC surface. Conversely, the restriction to the extended  $\triangle^2$ -net avoids the need to zoom-in into area of irregularity on a large model, see e.g. Fig. 9 a and emphasize problematic nets. The nodes of the  $\triangle^2$ -net shown Fig. 10 a are obtained from the planar layout



**Figure 10.** Comparing  $FC_8^3$  to variants FP7 and FF4, and to its predecessor  $FC^3$ . (a) Labels of extended  $\triangle^2$ -net, see also Fig. 2 a. The highlight line distribution improves from (c)–(f).

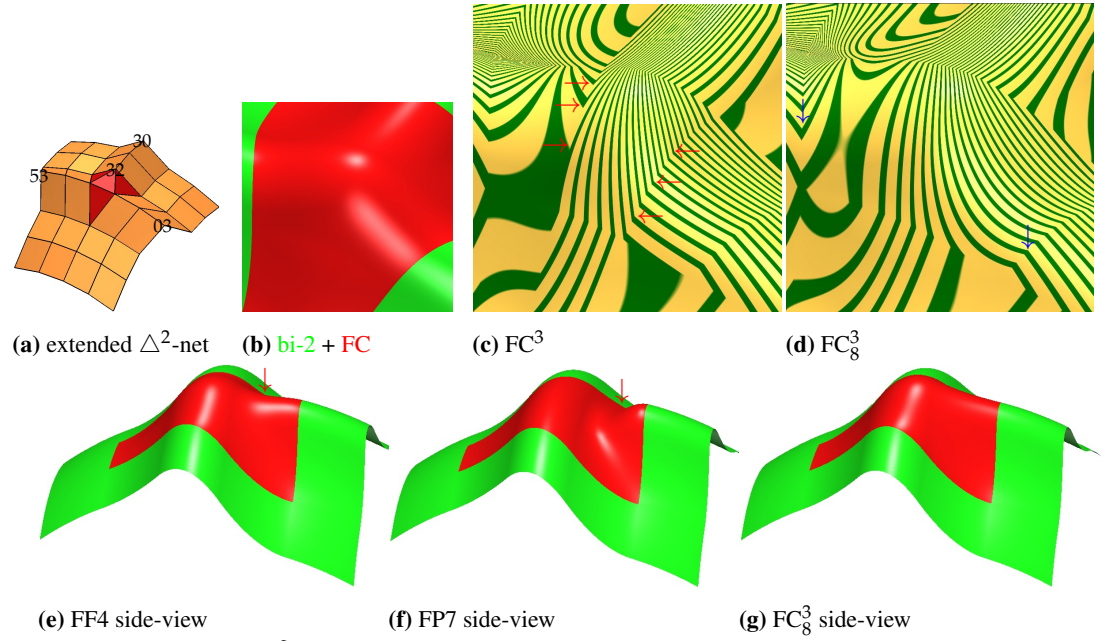
of Fig. 2 b by projection onto an elliptic paraboloid. This type of control net is a key when testing surfaces obtained from nets contracting as in Fig. 1 : a high quality surface, similar to an elliptic paraboloid within the region of Fig. 10 b is expected. FP7 displays undesired strong oscillation of the highlight lines, and FF4, as well as  $FC_8^3$  reveals no artifacts under scrutiny, justifying the subtle construction in [6]. Improving on  $FC^3$  is not expected in this specific hard configuration. However, Fig. 11 , Fig. 12 , Fig. 13 show an improvement of  $FC_8^3$  over  $FC^3$  in the highlight line distribution across the transition between patches 5 and 6, respectively and 7 and 8 (see Fig. 6 b for labels), likely due to the increased smoothness when combining the patches into one.

The extended  $\triangle^2$ -net of Fig. 11 a is derived from Fig. 10 a by lifting a 'horizontal' row of nodes (labels  $i3$ ,  $i = 0, \dots, 5$ ) and a 'vertical' triple ( $3j$ ,  $j = 0, 1, 2$ ) to 32: (b) displays the region shown in (c), (d). Red arrows in Fig. 11 c point to abrupt changes in highlight lines for  $FC^3$  that disappear in  $FC_8^3$ , while the  $\downarrow$  in Fig. 11 d points to sharper turns in the  $FC_8^3$  highlight lines than in same location for  $FC^3$ . The bottom row compares side-views revealing unexpected dips pointed by  $\downarrow$  of FF4 and FP7.

The extended  $\triangle^2$ -net of Fig. 12 is derived from Fig. 10 a by pushing down the nodes with labels  $ij$ ,  $j = 0, 1, 2$ . Red arrows in Fig. 12 c point to abrupt changes in highlight lines for  $FC^3$  that disappear in  $FC_8^3$ , while the  $\leftarrow$  in Fig. 12 d points to slightly sharper turns in the  $FC_8^3$  highlight lines than in same location for  $FC^3$ . The bottom row compares of side-views for  $FC_8^3$  and FP7, revealing an unwanted dip, pointed by  $\downarrow$ , in FP7. Fig. 13 adds a wavy  $\triangle^2$ -net commonly occurring in automatically generated meshes. Again,  $FC_8^3$  has a slight shape advantage over  $FC^3$  indicated by  $\leftarrow$ .

In summary, empirically, we see only a slight (if any) degradation of the highlight line distribution by using fewer pieces in  $FC_8^3$  over  $FC^3$  and an improvement of  $FC_8^3$  over  $FC^3$  in the highlight





**Figure 11.** Comparing  $FC_8^3$  to variants FP7 and FF4 for ridge preservation.

line distribution across the transition between the merged patches. That is, sharp turns either become considerably milder or disappear.

#### 4.2. Large hand-crafted models

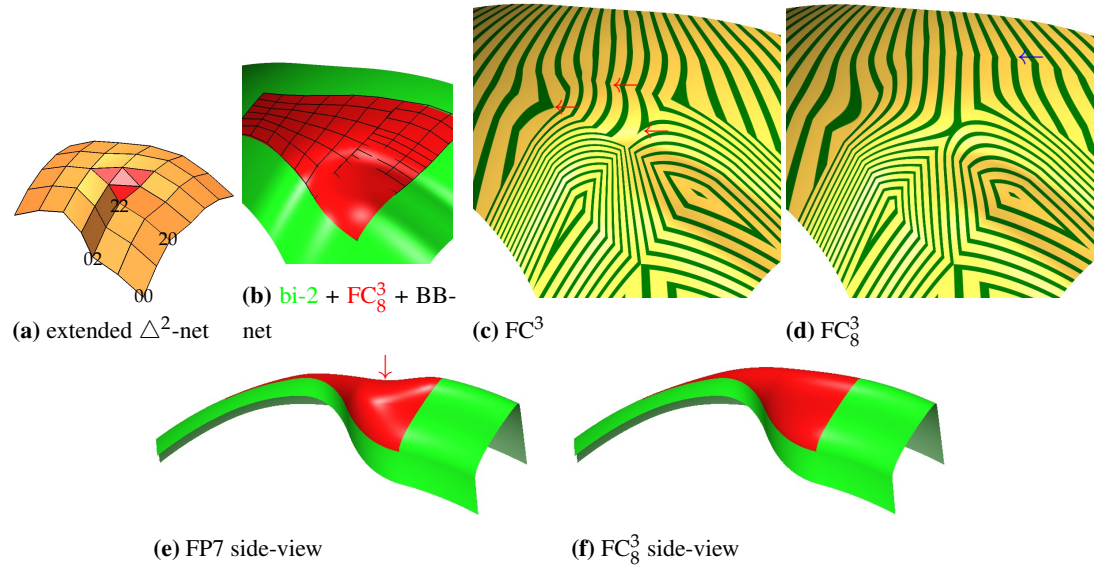
The original motivation of  $FC^3$  ( $FC^4$ ) was to address local challenges in *re-meshing* for spline surfaces. But the solution lends itself to *direct* design of larger objects, e.g. to design surfaces that start with the ubiquitous shape from revolution such as the examples in Fig. 14 (cf. Fig. 16).

Fig. 15 demonstrates design with  $\Delta^2$ -nets. The input (a) is a mesh of revolution: the nodes in the 10 horizontal rotational layers lie on co-axially stacked circles. The bottom 4 layers consist of 36 nodes each, the 5th has 24, the 6th and 7th have 12, the 8th layer 8, and the top two layers have 4 nodes each. The mesh is capped by a quad face, (b) shows the surface layout: the bottom 4 layers become **bi-2 patches**; the 12 lower and the 4 upper  $\Delta^2$ -nets become  $FC_8^3$  macro-patches; the four 3-valent vertex neighborhoods at the top are covered by bi-3 patches according to [36]. While the  $\Delta^2$ -nets overlap, their **cores** are sufficiently separated to build  $FC_8^3$  macro-patches. Note that (c) contains no sub-mesh defining a bi-2 patch. The second row zooms in on and displays the highlight line distribution of three challenging neighborhoods: (e,f) focuses on the transition between the 12 bottom and 4 top  $FC_8^3$  surfaces; (g,h) on the transition between the 4 top  $FC_8^3$  and the valence 3 neighborhoods; (i,j) on the transition between the regular **bi-2 patches** and the 12 bottom  $FC_8^3$ . The most noticeable changes in the highlight lines occur where regular bi-2  $C^1$  splines are used, as further discussed later with respect to Fig. 18 c. The bottom row illustrates hand-crafted designs, whose highlight line distributions are on par with regular bi-2 splines.

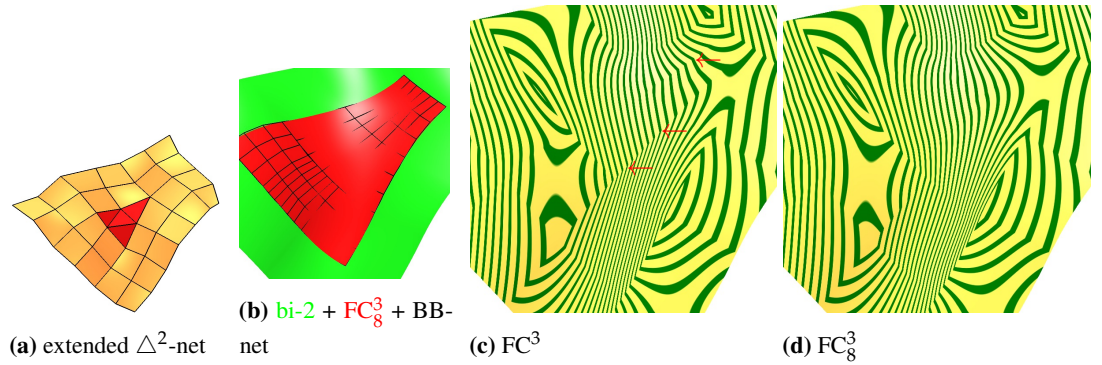
In Fig. 16 a the rapid merging part of quad strips with  $\Delta^2$ -nets is taken from Fig. 15 a, while the bottom part (now four quad strips) is modified anticipating a 'connecting tube'. The valence 5 vertices are treated with [36] to yield the smooth transitions in (b). Fig. 16 c,d show a design modification involving the  $\Delta^2$ -nets.

The goal of Fig. 17 is to compare  $FC_8^3$  for  $\Delta^2$ -nets to the less rapidly contracting bi-3 surfaces of [8] and to regular  $C^1$  bi-2 splines for designs where any of the three options can be chosen. That is, if  $FC_8^3$  looks no worse than its two alternatives, despite supporting rapid contraction,  $FC_8^3$  passes the test. We recall that [8] takes as input  $\tau_0$ -nets, namely triangles with two vertices of valence 4 and one with valence 5, surrounded by one layer of quad facets. Row 1 shows surfaces created using [8], and Row 2 regular bi-2 spline surfaces. To make the corresponding surfaces as similar as possible, the 10 layers of (a), (g) Fig. 17 lie on the same circles as for Fig. 15. The main change is the number of nodes in Fig. 17: in (a) layers 1, 2, 3, 4 have 32, layers 5, 6 have 16, layers 7, 8 have 8





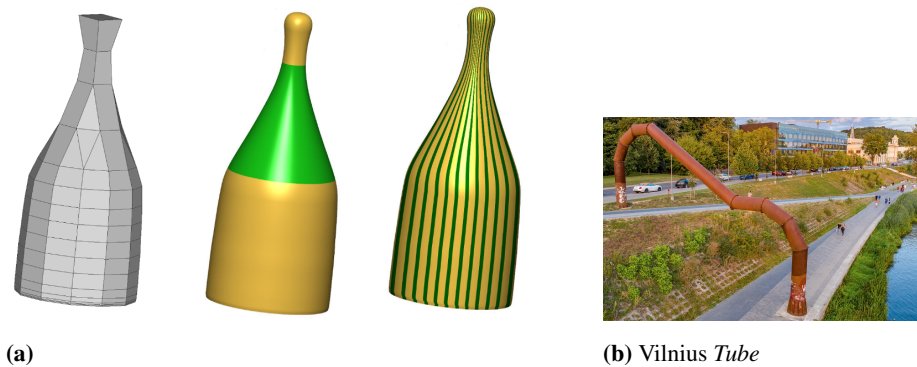
**Figure 12.** Comparing  $FC_8^3$  to  $FP_7$  and  $FC^3$  for step-like transition. (b) area of highlight line distribution in (c,d).



**Figure 13.** Comparing  $FC_8^3$  to  $FC^3$  on wave-like input.

and layers 9, 10 have 4 nodes; in (g) all layers have 36 nodes. Unlike (a), in the regular mesh (g) the top is not closed: the best option in terms of simplicity and quality) is to cap with 36 triangles sharing a common central vertex, i.e. a polar configuration, see [18] for the details. We omit this cap to focus on the comparison of regular splines with their counterparts based on  $\Delta^2$ - and  $\tau_0$ -nets. (Analogously, the cap from Fig. 15 b and Fig. 17 b is omitted displaying the corresponding surfaces in Fig. 17 n,o.) All surfaces in Fig. 15 b, Fig. 17 b,h have the same axial symmetries and similar highlight line distributions, see Fig. 17 m,n,o. That is the highlight line distributions depend on the geometry (large-scale flow) of input meshes more so than on the choice of construction. Modified surfaces can look alike as in Fig. 17 f and Fig. 16 d, or they can differ due to a different layout of  $\tau_0$  vs  $\Delta^2$  cores (gray in Fig. 1 a,f); see the bottom of Fig. 17 d vs Fig. 15 l. By contrast, the bottom of the regular bi-2 surface Fig. 17 j is very similar to Fig. 15 l; at the top the surface is less of a global shape modification than a local embossing since the corresponding layer in Fig. 15 a has 12, whereas Fig. 17 g has 36 nodes and in each case four nodes are displaced outwards (Fig. 17 k,l displacing by a smaller amount makes a local embossing milder, however an effect of global modification is not achieved). Achieving the effect of  $FC_8^3$  with the un-contracted net is a tricky challenge for a designer as is also if connecting un-contracted tube end to a single quad on the outer disk of Fig. 16.

Fig. 18 top compares the base of Fig. 15 l to the base of Fig. 17 j. The highlight line distributions in Fig. 18 b,c indicate similar surface quality. Also comparing the highlight line distribution of the mid-section, Fig. 18 e,f, shows no clear winner. Indeed, we observe in numerous tests that the quality of  $FC_8^3$  surfaces is no worse than the quality of regular  $C^1$  bi-2 splines, despite the reduction in degrees of freedom.



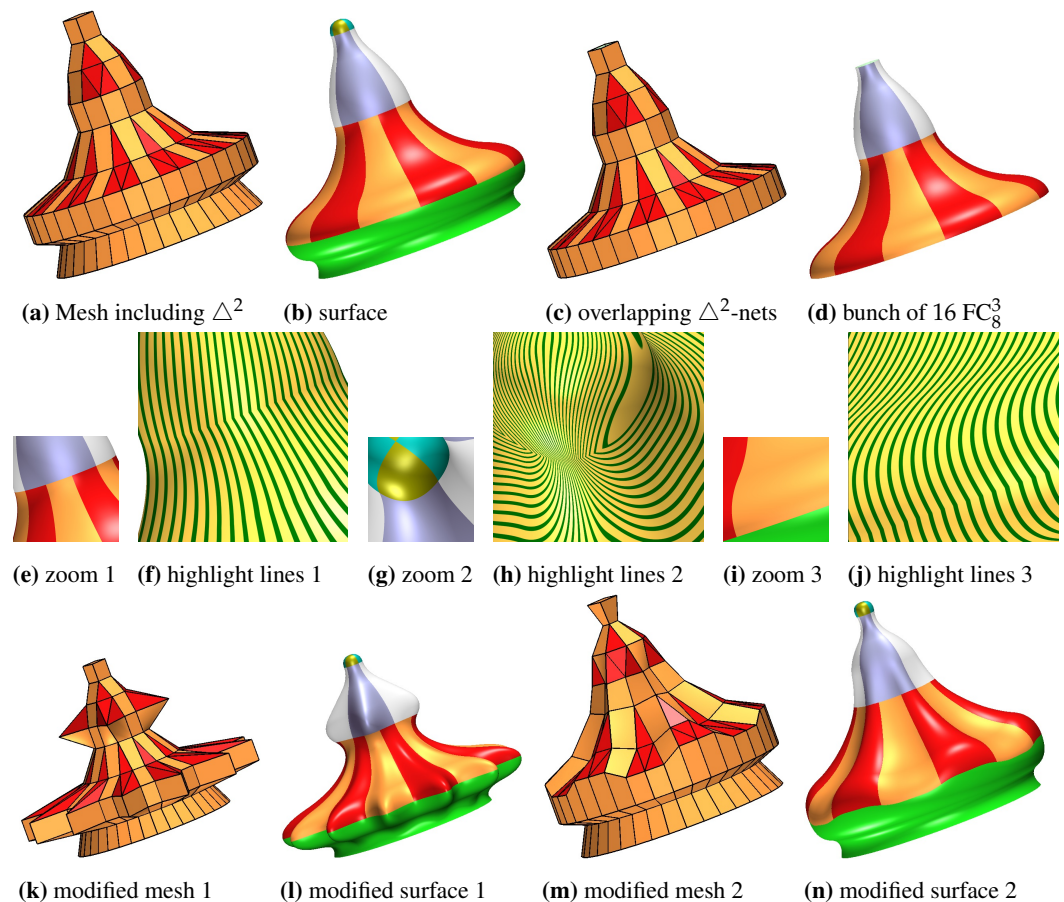
**Figure 14.** Natural occurrence of  $\Delta^2$ -nets in design. (a)  $FC_8^3$  is green. (b) Modern art installation

## 5. Conclusion

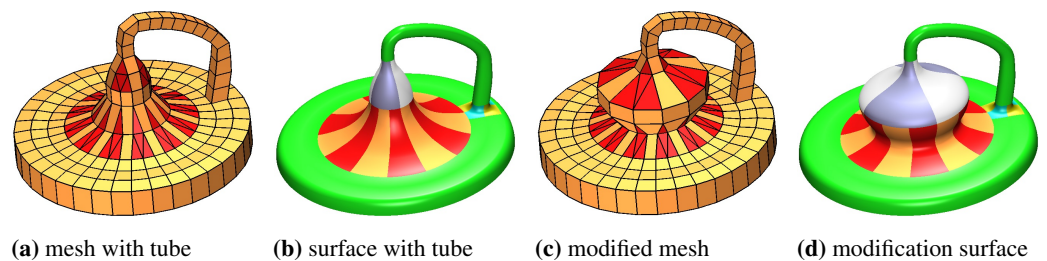
While very specialized, the optimal treatment of rapid contraction  $\Delta^2$ -nets by  $FC_8^3$  surfaces is an important building block that allows properly adjusting the parameterization of free-form surfaces when accommodating narrow passages or decrease of detail. Artificially comparing to  $\tau_0$ -surfaces and regular bi-2 splines where such rapid contraction is not needed shows the  $FC_8^3$  surfaces to be of equal quality and therefore to fit nicely into the Polyhedral-net Spline framework [35].

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**Figure 15.** Overlapping  $\Delta^2$  nets. (c) shows the sub-net of (a) that consists entirely of overlapping  $\Delta^2$ -nets. That is, the surface in (d) consists entirely of  $FC_8^3$  macro-patches.

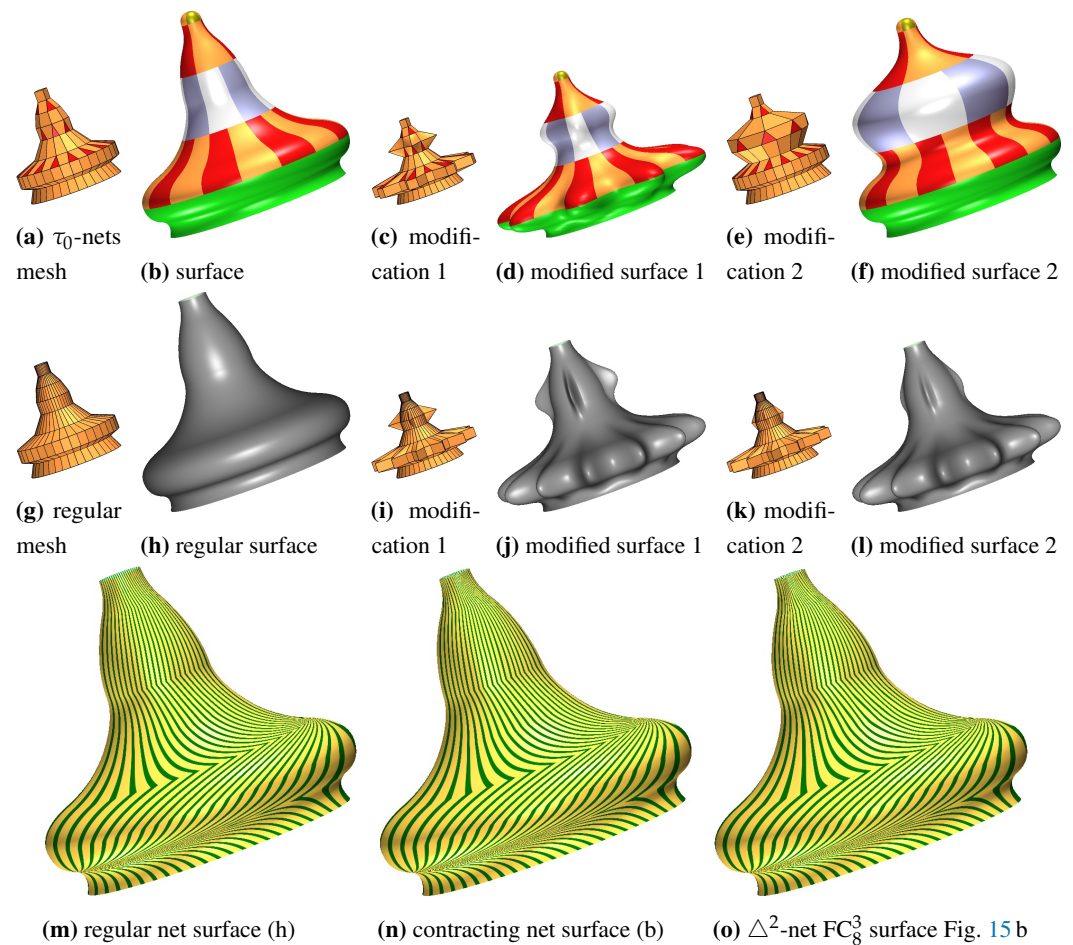


**Figure 16.** Design inspired by Fig. 14 b.

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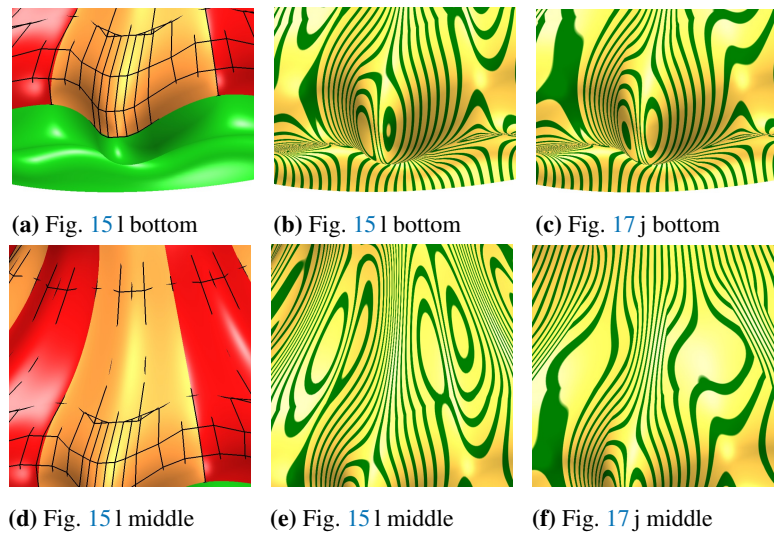
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(m) regular net surface (h) (n) contracting net surface (b) (o)  $\Delta^2$ -net  $FC^3$  surface Fig. 15 b  
**Figure 17.** Designs mimicking Fig. 15 but using  $\tau_0$ -nets or regular bi-2 splines. (m,n,o) visual equivalence of un-contracted, moderate-speed-contracted and fast-contracted surfaces.

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**Figure 18.** Detailed comparison of surfaces Fig. 15 (l) and Fig. 17 (j).

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